



Lakefront Heights Inc.

## Official Plan and Zoning By-Law Amendments

### **Functional Servicing Report**

Lakefront Heights Development  
Windsor, Ontario

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# Introduction

Dillon Consulting Limited (Dillon) was retained by Lakefront Heights Inc. to develop a functional servicing strategy for the potential development of their lands located on Wyandotte Street East, east of Clover Street, south of the existing Riverside Sportsmen Club in East Riverside, in the City of Windsor. This document outlines the servicing strategy and identifies the supporting studies and related information for the transportation, noise, sanitary, stormwater management, and watermain servicing for the site.

The development lands have been severed from the Riverside Sportsmen Club, located at 10835 Riverside Drive East, which is currently in operation as a private commercial club. The proposed development location is shown in Figure 1 below.



Figure 1: Project Site Location

The proposed development area is approximately 1.66 Ha and when fully developed, will consist of two multi-unit residential towers consisting of approximately 220 units total, and 18 attached townhome style units.

## 1.1

## References Documents

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The following documents and drawings were referenced when completing this study:

- City of Windsor – Development Manual (Windsor, 2015);
- City of Windsor – Sewer Atlas (City of Windsor);
- Design Guidelines for Sewage Works (MOE, 2008); and
- Windsor/Essex Region Stormwater Management Standards Manual (ERCA, 2018)

## 2.0

## Transportation Servicing

## 2.1

### Existing Conditions

Currently, there is no access to the development. A new access point will be required for the proposed development.

The property is bounded on the west limit by the East End Park, on the north by the Riverside Sportsmen Club, on the east by vacant lands and on the south by Wyandotte Street East.

## 2.2

### Proposed Roadways

The proposed access points to this development will be from a single driveway onto Wyandotte Street East.

The internal parking lot layout will service the proposed buildings. The parking lot will be designed to satisfy the City of Windsor's Development Manual. The proposed layout is shown in Figure 2 (in Appendix A)

The pavement structure of the proposed parking lot will be consistent with geotechnical recommendations.

A Traffic Impact Study (TIS) has been completed for this development by Dillon. Any impacts to the existing road network have been identified in that report and will be incorporated in the detailed design of this development.

## 3.0

## Sanitary Servicing

## 3.1

### Existing Conditions

Currently, there are no sanitary services to this property. An existing 250 mm diameter PVC sanitary sewer is located along Wyandotte Street East, and turns north at the Clover Ave intersection. Additionally, there is development to the south of Wyandotte Street East currently in progress which will consist of a 250 mm diameter PVC sanitary sewer on Lublin Avenue.

## 3.2

### Design Criteria

The following sanitary sewer design criteria for this property are outlined in Table 1.0. The design criteria were established by the City of Windsor's Development Manual (2015).

Table 1: Sanitary Sewer Design Criteria

Criteria	City of Windsor Development Manual
Hydraulic Sewer Sizing	Manning's Equation
Minimum Sewer Size (mm)	250 diameter
Minimum Cover Depth (m)	2.4
Maximum Manhole Spacing	90m preferred, maximum 120m
Manning's Roughness Coefficient 'n'	0.013
Velocity:	
Minimum (m/s)	0.75
Maximum (m/s)	3.00
Manning's Roughness Coefficient	0.013 (Smooth Wall Pipe)
Extraneous Flow	0.156 L/s/ha
Peaking Factor	6 (population under 1,000)
Population Density For:	
High Density Residential	2 person/unit
Average Daily Sewage	0.0042 L/second/capita
Sewer Surcharging	Maximum Hydraulic Grade Line

## 3.3

### Proposed Servicing

Figure 2 (in Appendix A) illustrates the proposed sanitary servicing layout. The sanitary servicing for the proposed development is as follows:

- All sanitary flows from within the proposed development will be conveyed via the local sanitary sewer constructed within the proposed internal parking lot.

- It is proposed that the local sanitary sewers that run east down Wyandotte Street East will be utilized via a single outlet to the proposed sanitary sewer on Lublin Avenue which will be installed prior to the development of this site.

The sanitary sewer functional design sheets are provided in Appendix B and assumes a full development build out. Criteria used in flow calculation is listed in Table 1.0.

The existing invert elevations of the sanitary trunk sewer allows for 2.4 m cover at the top end of the internal sewers. All serviced buildings where the bottom of the footings are below the sewer and the hydraulic grade line is less than 300 mm below the basement floor elevation, shall be equipped with a sewage ejector pump. It is recommended that all serviced buildings install sewage ejector pumps to provide a hydraulic break between the sewer and the building lot.

The future detailed design of the sanitary sewers and services are to be consistent with the requirements of the Ontario Building Code.



## 4.0

# Stormwater Servicing

## 4.1

## Background Information

An existing 1350 mm diameter RCP stormwater trunk sewer is located along the Wyandotte Street East right-of-way and ultimately discharges to the North Neighbourhood Pond. Currently there are no stormwater services to this property, however, this site has been allocated to the North Neighbourhood Pond.

## 4.2

## Design Criteria

The following storm sewer design criteria for this property are outlined in Table 2.0. The design criteria were established by the City of Windsor's Development Manual (2015).

Table 2: Storm Sewer Design Criteria

Criteria	City of Windsor Development Manual
Design Method	Rational Method
Standard Return Period	1 in 5 years Storm Event
Rainfall Intensity	$I = a / (t+b)^c$ $a=1259.0$ $b=8.80$ $c=0.838$
Minimum Cover Depth (m)	1.00
Manning's Roughness Coefficient 'n'	0.013
Velocity:	
Minimum (m/s)	0.76
Maximum (m/s)	3.00
Maximum Manhole Spacing	675mm diameter or less: 120 metres 750 to 1350mm diameter: 150 metres
Inlet Times: Residential	20 minutes (maximum)
Runoff Coefficients:	
Roofs	0.95
Road Pavements	0.90
Paved Driveways and Patios	0.90
Lawn – Sandy Soil	0.15
Lawn – Clay Soil	0.20
Parks	0.20
Gravel Lots	0.55
Minimum Manhole Size	1200mm
Pipe Material Main Lines	450mm or less: PVC or Reinforced Concrete Greater than 450mm: Reinforced Concrete (65-D min.)

Note: The detailed design for stormwater servicing will be completed with a dual drainage hydrodynamic model and will adhere to ERCA Guidelines.

## 4.3

## Proposed Servicing

It is proposed that the site's stormwater outlet be provided to the existing storm sewer on Wyandotte Street East, and discharged into the North Neighbourhood Pond located to the southwest of the proposed development.

Refer to Figure 2 (in Appendix A) for the proposed servicing. The stormwater servicing for the proposed development is as follows:

- The proposed buildings and parking lot will be serviced through a new storm sewer network constructed within the proposed parking lot;
- The proposed storm sewer network will outlet into the existing storm sewer on Wyandotte Street East, and discharge into the North Neighbourhood Pond located to the southwest of the proposed development. Refer to the Stormwater Management Report in Appendix C for details; and
- Stormwater quality control will be provided in the proposed stormwater management pond and parking lot surface storage. Details are provided in Appendix C.

## 5.0

## Watermain Servicing

## 5.1

### Existing Conditions

The site is not currently connected to a watermain service. There is an existing 400 mm diameter PVC watermain located to the south of the proposed development within the north side of the Wyandotte Street East right-of-way. The existing watermain is currently equipped with a stub which will be used to service the property.

## 5.2

### Proposed Servicing

Figure 2 (in Appendix A) illustrates the proposed watermain servicing. The watermain servicing for the proposed development is as follows:

- The internal development will be serviced by a new 200 mm diameter watermain constructed within the proposed internal parking lot network; and
- The new watermain will connect to the existing 400 mm diameter main located within the Wyandotte Street East right-of-way.

No pressure/flow testing has been completed for this development. During detailed design, pressure testing of the existing watermain on Wyandotte Street East may be required.

The detailed design of the watermain services are to be consistent with the requirements of the City of Windsor and will be coordinated with Windsor Utilities Commissions (W.U.C.) during the detailed design process. Placement of hydrants for adequate fire protection will be completed during detailed design.

6.0	<b>Utilities</b>
6.1	<b>Gas</b>  Existing natural gas service is available along Wyandotte Street East. During detailed design, future conversation on loading will be required with Enbridge.
6.2	<b>Bell</b>  Existing Bell service is available along Wyandotte Street East. During detailed design, future conversation will be required for servicing the proposed development.
6.3	<b>Cogeco</b>  Existing Cogeco service is available along Wyandotte Street East. During detailed design, future conversation will be required for servicing the proposed development.
6.4	<b>MNSi</b>  Existing MNSi service is available along Wyandotte Street East. During detailed design, future conversation will be required for servicing the proposed development.

## Conclusion

The review of the adjacent services is found to be sufficient for the proposed development. The design of the proposed internal services will be finalized during detailed design.

Yours sincerely,

DILLON CONSULTING LIMITED



Kyle Edmunds, P.Eng.  
Project Engineer

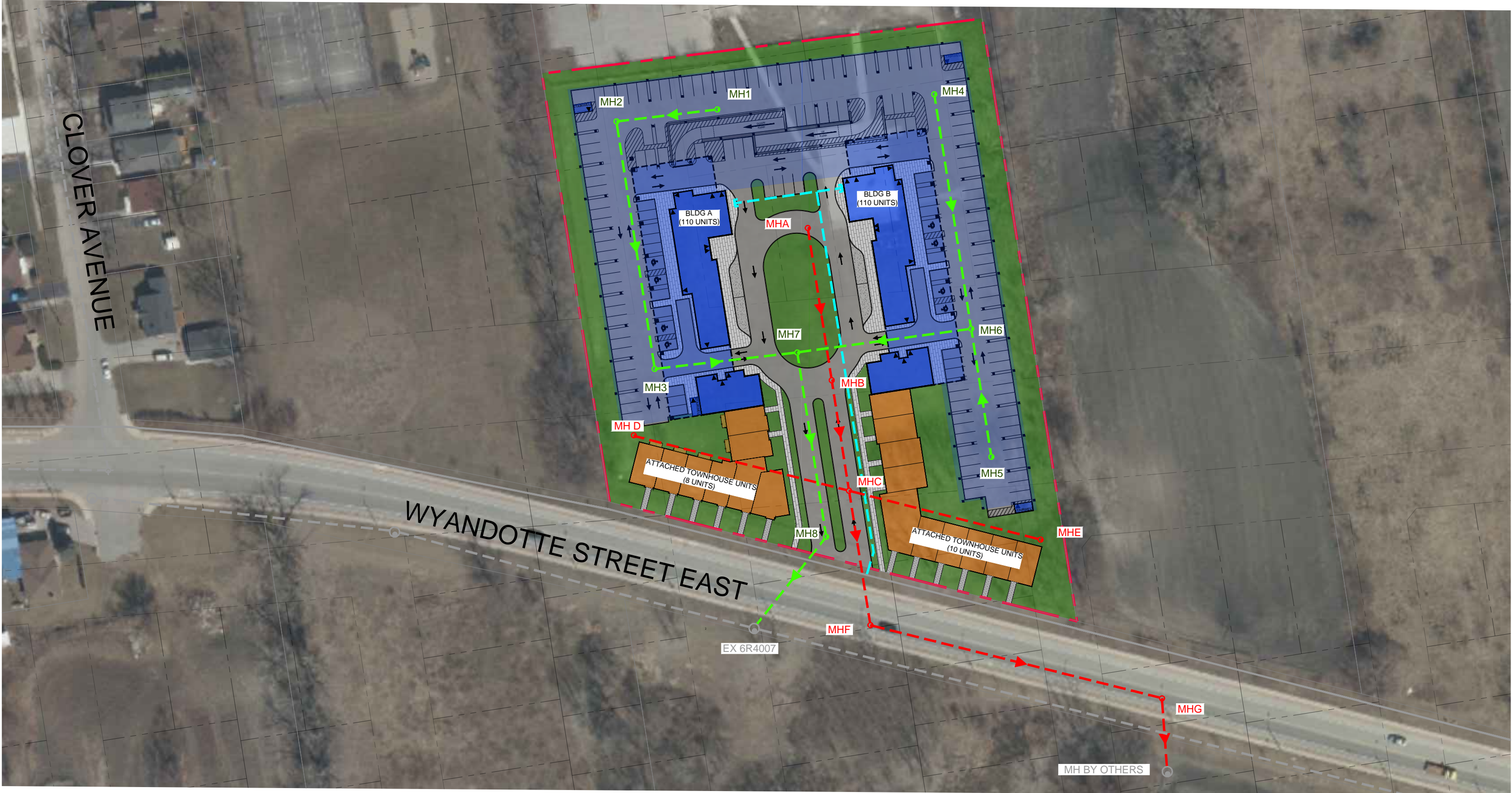


Kailee Dickson, EIT  
Civil Designer

## Appendix A

### ***Functional Servicing Plan***





LAKEFRONT HEIGHTS INC.  
10835 RIVERSIDE DRIVE EAST

FUNCTIONAL SERVICING PLAN  
FIGURE 1

SUBJECT AREA (± 1.66 ha / 4.11 ac)	PROPOSED MULTIPLE RESIDENTIAL BUILDING (220 UNITS)	PROPOSED TOWNHOME DWELLINGS (19 UNITS)	PROPOSED SIDEWALK	PROPOSED STORM SEWER	PROPOSED SANITARY SEWER	PROPOSED WATERMAIN
PROPOSED PAVEMENT	PROPOSED LANDSCAPE			PROPOSED STORM MH	PROPOSED SANITARY MH	EXISTING MH
				EXISTING SEWER		

File Location:  
c:\pw working directory\projects 2021\32kyd\dms32529\21-2104 sportsman club - servicing plan.dwg  
June, 14, 2024 10:57 AM

SOURCE: THE COUNTY OF ESSEX INTERACTIVE MAPPING (2019)

MAP/DRAWING INFORMATION  
THIS DRAWING IS FOR INFORMATION PURPOSES ONLY. ALL DIMENSIONS AND BOUNDARY INFORMATION SHOULD BE VERIFIED BY AN O.L.S PRIOR TO CONSTRUCTION.  
CREATED BY: KYD  
CHECKED BY: KNE  
DESIGNED BY: KYD

SCALE: 1:500

PROJECT: 21-2104  
STATUS: FINAL  
DATE: 06/14/2024

## Appendix B

### *Sanitary Sewer and Storm Sewer Design Sheets*



RIVERSIDE SPORTSMEN CLUB  
SANITARY SEWER DESIGN SHEET

Project Name: Riverside Sportsmen Club  
Project No: 21-1691

The Peaking Factor was derived:  
Using Harmon Formula= N (Y or N)  
From a Table= Y  
Value from table= 6.000

Residential Average Daily Flow= 363 L/Cap.D  
Peak Extraneous Flow= 0.156 L/Ha.S

Outlet Invert Elevation= 173.295

Mannings 'n'= 0.013

City of Windsor

Total Area= 1.899

Location			Flow Characteristics								Sewer Design/Profile								
ROAD/STN	LOCATION		INDIVIDUAL		CUMULATIVE		PEAKING FACTOR M	POP FLOW Q(p) (L/s)	PEAK EXTR. FLOW Q(i) (L/s)	PEAK DESIGN FLOW Q(d) (L/s)	CAPACITY (L/s)	LENGTH (m)	PIPE DIA. (mm)	SLOPE (%)	UPPER INVERT (m)	LOWER INVERT (m)	FALL (m)	VELOCITY (m/s)	DROP IN LOWER MANHOLE (m)
	FROM MH	TO MH	POP	AREA (ha.)	POP	AREA (ha.)													
Parking Lot	A	B	440	0.99	440	0.99	6.000	11.088	0.154	11.24	59.47	41.3	250	1.00	174.334	173.921	0.413	1.21	0.000
Parking Lot	B	C	12	0.43	452	1.42	6.000	11.390	0.222	11.61	36.66	30.0	250	0.38	173.921	173.807	0.114	0.75	0.000
Behind Homes	D	C	12	0.10	12	0.10	6.000	0.302	0.016	0.32	59.47	59.7	250	1.00	174.404	173.807	0.597	1.21	0.000
Behind Homes	E	C	12	0.10	12	0.10	6.000	0.302	0.016	0.32	59.47	55.0	250	1.00	174.357	173.807	0.550	1.21	0.000
Parking Lot	C	F	0	0.08	476	1.71	6.000	11.995	0.267	12.26	36.66	36.3	250	0.38	173.807	173.669	0.138	0.75	0.000

RIVERSIDE SPORTSMEN CLUB  
STORM SEWER DESIGN SHEET

Project Name: Riverside Sportsmen Club  
Project Number: 21-2104

Intensity Option # 1  
1) Intensity (i) = a/(t+b)^c      2) Intensity (i) = a\*t^b      3) Insert Intensity

Based on 1:5 Year Storm Event  
Windsor, Ontario

a= 1259.000      a=      i=      b= 8.800      b=      c= 0.838

Manning's n = 0.013  
Total Area (ha)= 1.67      Outlet Invert Elevation= 172.055

Location											Sewer Design / Profile								
From MH	To MH	Area (ha)	Run. Coef.	2.78AC	Accum. 2.78AC	T of In (min)	T of F (min)	T of Conc. (min)	Intensity (mm/hr)	Exp. Flow (L/s)	Capacity (L/s)	Velocity (m/s)	Length (m)	Pipe Dia. (mm)	Slope (%)	Invert Up MH	Invert Low MH	Fall (m)	Drop Across Low MH (m)
MH 1	MH 2	0.25	0.90	0.63	0.63	15.0	0.60	15.00	88.40	56.11	84.09	0.76	27.2	375	0.23	172.529	172.466	0.06	0.025
MH 2	MH 3	0.32	0.90	0.81	1.44		1.42	15.60	86.59	124.76	172.02	0.79	67.6	525	0.16	172.441	172.333	0.11	0.025
MH 3	MH 7	0.10	0.90	0.24	1.68		0.76	17.01	82.58	138.97	182.46	0.84	38.5	525	0.18	172.308	172.239	0.07	0.025
MH 4	MH 6	0.30	0.90	0.76	0.76	15.0	1.40	15.00	88.40	66.97	84.09	0.76	63.9	375	0.23	172.500	172.353	0.15	0.025
MH 5	MH 6	0.27	0.90	0.67	0.67	15.0	0.76	15.00	88.40	59.08	84.09	0.76	34.7	375	0.23	172.433	172.353	0.08	0.025
MH 6	MH 7	0.13	0.90	0.32	1.75		0.91	16.40	84.27	147.17	187.46	0.87	47.1	525	0.19	172.328	172.239	0.09	0.025
MH 7	MH 8	0.17	0.90	0.43	3.86		0.92	17.78	80.60	310.78	401.40	0.91	50.0	750	0.13	172.214	172.149	0.06	0.025
MH 8	6R4007	0.12	0.90	0.31	4.17		0.55	18.69	78.34	326.54	416.55	0.94	31.3	750	0.14	172.124	172.080	0.04	0.025

## Appendix C

### *Stormwater Management Report*



Lakefront Heights Inc.

## Official Plan and Zoning By-Law Amendments

Stormwater Management Report

Lakefront Heights Development

Windsor, Ontario

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## Appendices

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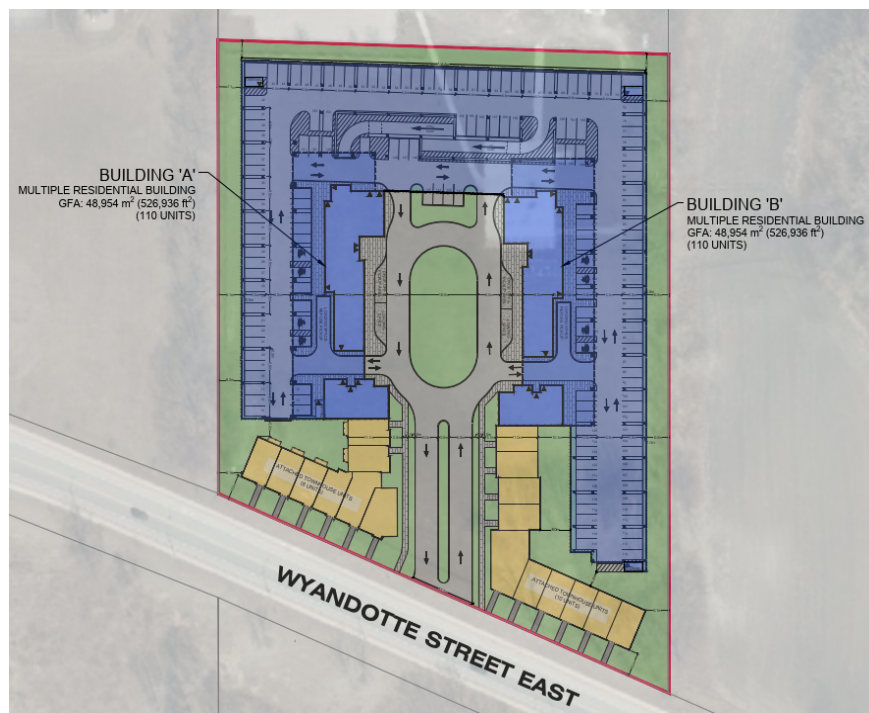
- A Lakefront Heights Concept Plan
- B Modelling Input and Output Reports
- C Details of OGS Unit
- D Wyandotte Street East Trunk Sewer Profile Comparison

## 1.0

# Introduction

Dillon Consulting Limited (Dillon) has been retained by Lakefront Heights Inc. to prepare a Stormwater Management Report in support of its Official Plan (OPA) and Zoning By-law Amendments (ZBA) for its proposed development to the south of the existing Riverside Sportsman Club. As shown in **Figure 1**, the proposed development is located in the neighborhood of East Riverside, in the City of Windsor, north of Wyandotte Street East.

The proposed development area is approximately 1.66 ha and is currently vacant undeveloped land, with the exception of a concrete pad located at the northeast corner of the site. The proposed development consists of a combination of multi-storey and attached townhome style residential buildings. The site plan for the proposed development can be found in **Appendix A**.



**Figure 1: Proposed Development**

## 1.1

## Background

In 2018, Dillon completed a stormwater assessment study of the North Neighbourhood Development for the City of Windsor (the City). The details of the previously completed study can be found in the North Neighbourhood Development Storm Water Management Analysis Report (Dillon 2018). The current development was part of the ultimate future build out area considered in the 2018 study. As such, the currently proposed development was assessed to the North Neighbourhood Stormwater Management

Pond and the Wyandotte Street East Trunk Sewer.

## 1.2 Stormwater Management Design Criteria

Design criteria for the stormwater design and servicing were based on review of the following reference documents:

- Stormwater Management Planning and Design Manual (Ministry of the Environment [MECP], 2003);
- Windsor/Essex Region Stormwater Management Standards Manual (WERSMSM) (2018); and
- North Neighbourhood Stormwater Management Study (Dillon, 2018).

The corresponding criteria are described below.

### 1.2.1 Quantity Control

The proposed SWM plan is designed at a minimum to provide active storage volume for the 100-Year, 24 hour storm and the 100-Year, 4 hour storm.

#### 1.2.1.1 Minor System Conveyance

The proposed site storm sewers are designed to accommodate the peak flows from the 5-Year design storm event.

#### 1.2.1.2 Major System Conveyance

The proposed major system is designed to limit the maximum surface ponding depths on the proposed roadways to 0.30 m.

#### 1.2.1.3 Climate Change Resiliency Assessment

The regional SWM facility is designed to accommodate the runoff generated from the Urban Stress Test design storm event without overtopping its banks.

### 1.2.2 Quality Control

On-site stormwater quality treatment will be provided using an oil-grit separator (OGS) positioned upstream of the outlet to the Wyandotte Street Trunk Storm Sewer. The OGS unit is designed to meet the Ministry of Environment, Conservation and Parks (MECP) design requirements for 70% TSS removal (normal level of protection). Additionally, the North Neighbourhood SWM facility (North Neighbourhood Pond) is designed to provide for a “Normal” Protection Level of water quality treatment to remove 70% of total suspended solids (TSS) from the proposed site runoff.



## 2.0

## Existing Conditions

The subject property is currently vacant undeveloped land, with the exception of a concrete pad located at the northeast corner of the site. The site is bound by the Riverside Sportsman Club to the north, Wyandotte Street East to the south, and vacant land to the east and East End Park to the west.

## 2.1

### Existing Drainage

Based on the available topographic information, runoff from the existing site generally travels south towards Wyandotte Street East as shallow surface flow. Flow from the site is entering the Wyandotte Street East Trunk Sewer where it ultimately discharges to the North Neighbourhood Pond. No external drainage areas contribute runoff to the site.

## 2.2

### Site Soils

Based on the information presented on the Soil Map of Essex County, the site soils of the site consist of Clyde Clay and Colwood Fine Sandy Loam. These soils are classified in the Ontario Agricultural Atlas as Hydrologic Soil Group (HSG) D and C, respectively.

## 2.3

### Tailwater Conditions

The impact of downstream tailwater conditions occurring against the site's stormwater management system was accounted for in this analysis. Head time-series were extracted from the North Neighbourhood Model for the 5-Year, 4 hour; 100-Year, 4 hour; 100-Year, 24 hour and UST events, for the node MH 6R4007. These time-series were then applied to the outfall node to represent tail water conditions.

The head time series used to simulate tailwater conditions for different storm events are shown below in **Figure 2**.

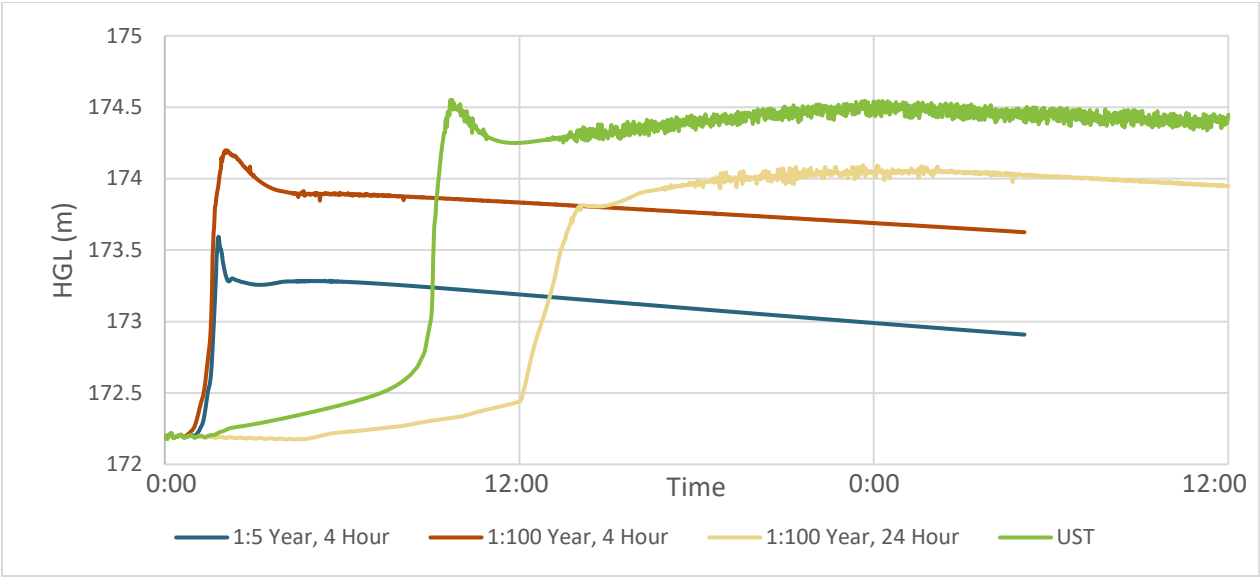


Figure 2: Tailwater time-series for various storm events

## 3.0 Proposed Condition Analysis

The proposed site development is 1.66 ha site area and consists of a combination of multi-storey and townhome residential buildings. All runoff from the proposed development is discharged to the North Neighbourhood Pond through the Wyandotte Street East Trunk Sewer. The site plan for the proposed development can be found in **Appendix A**.

### 3.1 Proposed Condition Hydrologic Assessment

Sub catchment attributes for the proposed development model were selected based on the ERCA SWM standard and are summarized in **Table 1** below. Additional details of the modelling parameters and other model details for proposed conditions are provided in **Appendix B**.

**Table 1: Post Development Sub-Catchment Parameters for the Site**

Attribute	Development
Land Use	Residential
Area (ha)	1.66
Flow Length <sup>1</sup> (m)	155
Imperviousness (%)	90
Slope (%)	1.5
Manning's n Impervious	0.013
Manning's n Pervious	0.24
Depression Storage Impervious (mm)	2.5
Depression Storage Pervious (mm)	7.5
Soil Capillary Suction Head (mm) <sup>2</sup>	215
Hydraulic Conductivity (mm/hr) <sup>2</sup>	1.15
Initial Soil Moisture Deficit (frac.) <sup>2</sup>	0.235

<sup>1</sup>Maximum flow path to outlet

<sup>2</sup>Weighted average for soil type C & D

### 3.2 Allowable Release Rate

The subject development lands were assessed to the Wyandotte Street East Trunk Sewer in the 2018 North Neighbourhood Study. In the 2018 report, the development lands were included with an

imperviousness percentage of 37% flowing unrestricted through overland flow to the Wyandotte Street East Trunk Sewer.

As such, the allowable release rate of the proposed site was estimated considering a percentage imperviousness of 37% in the modelling analysis. The estimated maximum allowable stormwater release rate for the development site is 160 L/s. This flow represents the 5-Year, 4 hour design storm event, peak flow rate from the development site using a 37% imperviousness for the site.

In order to prevent any adverse impacts on the downstream system due to the proposed development, the maximum flow rate from the site is expected to be maintained at or below the allowable release rate for all events up to and including the 100-Year event.

### 3.3 Preliminary SWM Strategy

A preliminary SWM strategy was developed to manage the runoff from the proposed site. The proposed strategy includes:

- An on-site storm sewer to convey the minor flows from all storms up to and including 5-Year design storm event;
- Catchbasin pre-treatment measures to capture oil and suspended sediment at the source;
- An oil/grit separator to provide water quality treatment;
- A gravity outlet with a flap gate to discharge the proposed site runoff to the Wyandotte Street East Trunk Sewer under high tailwater conditions; and
- On-site temporary stormwater storage to attenuate the peak discharges.

### 3.4 Storm Sewer Design

The proposed site storm sewers are designed to convey the site runoff to the Wyandotte Street East Trunk Sewer by gravity. The storm sewers are designed to accommodate the peak discharges from the 5-Year storm event. The peak discharge from the proposed storm sewer to the Wyandotte Street East Trunk Sewer is restricted by an orifice that limits the site discharge to the allowable release rate of 160 L/s.

### 3.5 Quantity Control

Stormwater storage on site is proposed by a combination of underground storage and above ground storage at catch-basin (CB) locations. A 750 mm diameter pipe and 230 mm circular orifice is proposed from the site to the outlet node (6R4007) to restrict the flow within the allowable rate.

The parking lot areas will be graded to include local sags at catch basin locations to allow for surface ponding during large storm events. Storage in the storm sewers and sewer structures has been taken into account in this analysis and incorporated into the stage-storage curve used to simulate on-site storage in the model.

The proposed condition model was simulated for different storm events. A summary of the release rates and the on-site storage volumes for various storm event simulations is provided in **Table 2**.

**Table 2: Onsite Storage Depth, Storage Volume and Release for Various Storms**

Storm Type	Release Rate (L/s)	Storage Volume (m <sup>3</sup> )
5-Year, 4 hour Chicago	130	390
100-Year, 4 hour Chicago	160	670
100-Year, 24 hour SCS Type-II	120	390
Urban Stress Test	120	990

Shown in **Table 2**, it is observed that the release rates for all simulated storm events is within the allowable limit of 160 L/s. It is also observed in the 100-Year, 4 hour storm (Chicago) event is the governing 100-Year return period event regarding storage requirements. The maximum volume of storm water estimated to be stored on-site is 670 m<sup>3</sup>, during the governing 100-Year simulation. The details of the model inputs and outputs are provided in **Appendix B**.

The Urban Stress Test (UST) storm event was also simulated to account for impacts of climate change. The estimated storage volume during the UST event simulation, shown in **Table 2**, is 990 m<sup>3</sup>, which is higher than the maximum estimated volume during the governing 100-Year simulation.

The maximum depth of storage on-site during the 100-year and UST events will be confirmed during detailed design stage.

The flow from the site is conveyed via a 750 mm diameter conduit to the outfall (6R3879) of the Wyandotte Street East Trunk Sewer. Additionally, a 230 mm circular orifice is required to restrict the flow within the allowable limit.

### 3.6 Quality Control

Water quality treatment is provided by a multi-component approach that includes:

- Pre-treatment measures in the proposed site catch basins to capture TSS; and
- An oil/grit separator (OGS) to meet the design TSS removal rate.

Pre-treatment devices will be selected during detailed design but must be designed to convey flows under freezing conditions. The site will require an OGS unit to meet Normal Protection Level water quality treatment to remove 70% TSS from the proposed site runoff. The FD-5HC model supplied by ADS, or approved equivalent is recommended for this site. The details of this OGS sizing is provided in **Appendix C**.

### 3.7 Downstream Capacity Analysis

The PCSWMM model developed as part of the North Neighbourhood Stormwater Management Study (Dillon, 2018) was utilized to determine upstream and downstream impacts on the Wyandotte Street East Trunk Sewer. The model was simulated using the 5-Year, 4 hour; 100-Year 4 hour; 100-Year 24 hour and the UST design storm events, with and without the inflow from the proposed development. Comparing the HGL through the Wyandotte Street East Trunk Sewer, there was no observed increase in HGLs during the storm events.

This is understood to be because the flows from the proposed development are relatively small in comparison to the peak flows in the larger Wyandotte Street East Trunk Sewer.

Therefore, it was concluded that the release rate from the proposed site is not expected to have a significant impact on the receiving sewer system. Profiles of the Wyandotte Street East Trunk Sewer showing the HGL, with and without the new development inflow, are included in **Appendix D**.

## 4.0

## Conclusions

The stormwater management design for the proposed development meets the established SWM criteria for the overall site, and no negative impacts due to the site development are anticipated in the existing system.

Based on the analysis performed, the conclusions are listed as follows:

- The allowable release rate for this proposed development is estimated to be 160 L/s. This is based on a 5-Year year pre-development release from the development area, assuming a pre-development percentage imperviousness of 37% for the site.
- A 750 mm diameter circular pipe and 230 mm diameter circular orifice is proposed at the outlet to provide flow restriction for maintaining outflow within the allowable release rate.
- Approximately 390 m<sup>3</sup> of underground storage is required to restrict flow from the site to the allowable release while maintaining the HGL below the road elevation for storms up to and including the 5-Year event.
- On-site storage volume of 670 m<sup>3</sup> is required for the 100-Year event to restrict flows from the site to the allowable release rate without surface ponding exceeding 0.30 m.
- From the outlet capacity assessment analysis, no significant change in HGLs in the Wyandotte Street East Trunk Sewer, downstream of the development, is observed. Therefore, no negative impact to the hydraulic conditions of the downstream municipal sewer is expected due to the proposed development.

This report is respectfully submitted for review and approval. Should you have any questions, we would be pleased to discuss the results of our evaluation in further detail.

Yours sincerely,

**DILLON CONSULTING LIMITED**



Aakash Bagchi, P.Eng. M.Eng.,  
Water Resources Engineer

Saranya Jeyalakshmi  
Water Resources Designer

# Appendix A

## *Lakefront Heights Concept Plan*

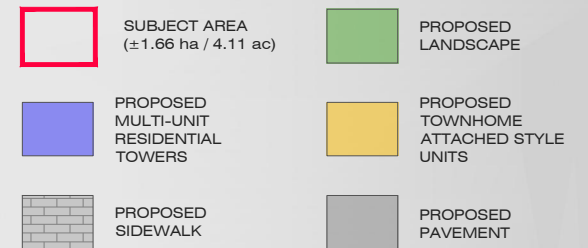


**BUILDING 'A'**  
MULTIPLE RESIDENTIAL BUILDING  
GFA: 48,954 m<sup>2</sup> (526,936 ft<sup>2</sup>)  
(110 UNITS)

**BUILDING 'B'**  
MULTIPLE RESIDENTIAL BUILDING  
GFA: 48,954 m<sup>2</sup> (526,936 ft<sup>2</sup>)  
(110 UNITS)

**WYANDOTTE STREET EAST**

**LAKEFRONT HEIGHTS INC.**  
LAKEFRONT HEIGHTS DEVELOPMENT  
PLANNING JUSTIFICATION REPORT  
**CONCEPTUAL DEVELOPMENT PLAN**  
GROUND FLOOR - PARKING LAYOUT  
FIGURE 4 (a)



SITE DATA MATRIX			
	ZONING PROVISIONS	REQUIRED	PROVIDED
1	PROJECT DESCRIPTION	N/A	RESIDENTIAL
2	ZONING DESIGNATION	RD3.3	SITE SPECIFIC RD3.3
3	LAND USE	N/A	RESIDENTIAL
4	MAJOR OCCUPANCY(S)	N/A	RESIDENTIAL
5	PERMITTED USES	MULTIPLE DWELLING	MULTIPLE DWELLING
6	MINIMUM SITE AREA	11,680m <sup>2</sup>	16,633m <sup>2</sup>
7	BUILDING AREA (GROUND FLOOR FOOTPRINT)	N/A	9,314.5m <sup>2</sup>
8	TOTAL UNITS	N/A	238
9	LOT COVERAGE	35%	56%*
10	MINIMUM LOT WIDTH	45.0m	129.4m
11	MAXIMUM BUILDING HEIGHT	24.0m	44.0m*
12	MINIMUM FRONT YARD DEPTH	N/A	6.0m
13	MINIMUM REAR YARD DEPTH	N/A	5.0m
14	MINIMUM SIDE YARD DEPTH	N/A	6.0m
15	REQUIRED SPACES - STANDARD	289	307
16	REQUIRED SPACES - ACCESSIBLE	8 (4 TYPE A AND 4 TYPE B)	16 (8 TYPE A & 8 TYPE B)
17	REQUIRED SPACES - VISITOR (15%)	44	48
18	PARKING SPACES - TOTAL	297	323
19	GROUND FLOOR PARKING	N/A	162
20	SECOND FLOOR PARKING	N/A	161
21	BICYCLE SPACES	18	23
22	LOADING SPACES	4	4
23	LANDSCAPED AREA - SOFT	N/A	4,871m <sup>2</sup>
24	LANDSCAPED AREA - HARD	N/A	1,159m <sup>2</sup>
25	LANDSCAPED AREA - TOTAL	35%	6,030m <sup>2</sup> (36.2%)
26	DWELLING UNITS PER HECTARE	180	144

\* REQUIRES SITE SPECIFIC ZONING BY-LAW AMENDMENT

SCALE : 1:750

SOURCE: COUNTY OF ESSEX  
AERIAL PHOTOGRAPHY (2021)

MAP/DRAWING INFORMATION  
THIS DRAWING IS FOR INFORMATION PURPOSES ONLY. ALL DIMENSIONS  
AND BOUNDARY INFORMATION SHOULD BE VERIFIED BY AN O.L.S PRIOR TO  
CONSTRUCTION.

CREATED BY: SNP  
CHECKED BY: MAM  
DESIGNED BY: SNP

File Location:  
c:\pw working directory\projects 2021\32mam\dms32529\21-2104 -sportsman club  
- site plan.dwg  
June, 14, 2024 9:39 AM



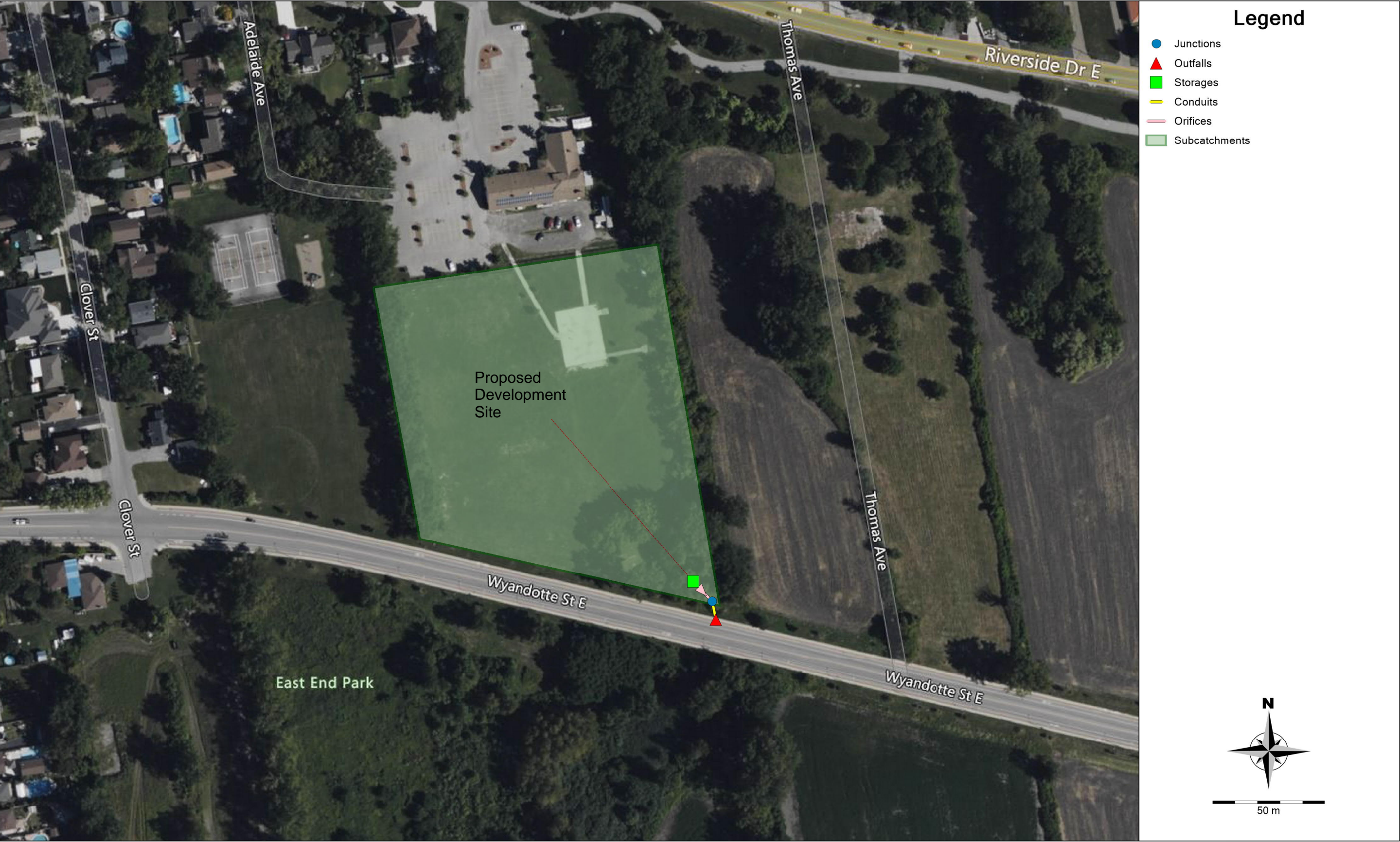
PROJECT: 21-2104  
STATUS: DRAFT  
DATE: 12/06/2024

## Appendix B

### *Modelling Input and Output Reports*



Model Schematic



# PCSWMM Input Report: 1:5 year 4 hour

[TITLE]

::Project Title/Notes

[OPTIONS]

::Option	Value
FLOW_UNITS	LPS
INFILTRATION	MODIFIED_GREEN_AMPT
FLOW_ROUTING	DYNWAVE
LINK_OFFSETS	ELEVATION
MIN_SLOPE	0
ALLOW_PONDING	NO
SKIP_STEADY_STATE	NO
START_DATE	10/13/2022
START_TIME	00:00:00
REPORT_START_DATE	10/13/2022
REPORT_START_TIME	00:00:00
END_DATE	10/14/2022
END_TIME	00:00:00
SWEEP_START	01/01
SWEEP_END	12/31
DRY_DAYS	0
REPORT_STEP	00:01:00
WET_STEP	00:05:00
DRY_STEP	00:05:00
ROUTING_STEP	5
RULE_STEP	00:00:00
INERTIAL_DAMPING	PARTIAL
NORMAL_FLOW_LIMITED	BOTH
FORCE_MAIN_EQUATION	H-W
VARIABLE_STEP	0.75
LENGTHENING_STEP	0
MIN_SURFAREA	0
MAX_TRIALS	8
HEAD_TOLERANCE	0.0015
SYS_FLOW_TOL	5
LAT_FLOW_TOL	5
MINIMUM_STEP	0.5
THREADS	6

[EVAPORATION]

```
;;Data Source      Parameters
;;-----
CONSTANT           0.0
DRY_ONLY           NO
```

[RAINGAGES]

```
;;Name            Format      Interval SCF      Source
;;-----
100Y4hr_Chicago  INTENSITY 0:15      1.0      TIMESERIES 100Y4hr_Chicago
100YrSCS          INTENSITY 2:00      1.0      TIMESERIES 100YrSCS
5Y4hr_Chicago    INTENSITY 0:15      1.0      TIMESERIES 5Y4hr_Chicago
UST               INTENSITY 0:15      1.0      TIMESERIES UST
```

[SUBCATCHMENTS]

```
;;Name            Rain Gage      Outlet      Area      %Imperv  Width      %Slope  CurbLen  SnowPack
;;-----
SM1               5Y4hr_Chicago  SMS1        1.66      90        107.097  1.5      0
```

[SUBAREAS]

```
;;Subcatchment    N-Imperv  N-Perv      S-Imperv  S-Perv      PctZero  RouteTo  PctRouted
;;-----
SM1               0.013    0.24        2.5       7.5         0        OUTLET
```

[INFILTRATION]

```
;;Subcatchment    Param1     Param2     Param3     Param4     Param5
;;-----
SM1               215        1.15       0.235      0          0
```

[JUNCTIONS]

```
;;Name            Elevation  MaxDepth    InitDepth  SurDepth    Aponded
;;-----
SMMH1            173.524    1.976       0          0          0
```

[OUTFALLS]

```
;;Name            Elevation  Type          Stage Data      Gated  Route To
;;-----
SMOF1            171.755    TIMESERIES TW_5YR_4Hr_NorthNeighbourHood NO
```

[STORAGE]

```
;;Name            Elev.      MaxDepth    InitDepth  Shape      Curve Name/Params      N/A      Fevap  Psi
Ksat      IMD
```

```

;;-----
-----
SMS1      173.524  1.976      0      TABULAR      Storage      0      0

[CONDUITS]
;;Name      From Node      To Node      Length      Roughness      InOffset      OutOffset      InitFlow      MaxFlow
;;-----
-
SMC1      SMMH1      SMOF1      10      0.013      173.524      173.324      0      0

[ORIFICES]
;;Name      From Node      To Node      Type      Offset      Qcoeff      Gated      CloseTime
;;-----
SMO1      SMS1      SMMH1      SIDE      173.524      0.65      NO      0

[XSECTIONS]
;;Link      Shape      Geom1      Geom2      Geom3      Geom4      Barrels      Culvert
;;-----
SMC1      CIRCULAR      0.565      0      0      0      1
SMO1      CIRCULAR      0.23      0      0      0

[LOSSES]
;;Link      Kentry      Kexit      Kavg      Flap Gate      Seepage
;;-----
SMC1      0      0      0      YES      0

[CURVES]
;;Name      Type      X-Value      Y-Value
;;-----
Storage      Storage      0      570
Storage      0.675      570
Storage      0.676      0.7
Storage      1.676      0.7
Storage      1.976      4500

[TIMESERIES]
;;Name      Date      Time      Value
;;-----
100Y4hr_Chicago      0:00      3.95
100Y4hr_Chicago      0:15      4.87
100Y4hr_Chicago      0:30      6.36
100Y4hr_Chicago      0:45      9.19

```



100Y4hr_Chicago	1:00	16.45
100Y4hr_Chicago	1:15	46.45
100Y4hr_Chicago	1:30	143.67
100Y4hr_Chicago	1:45	32.45
100Y4hr_Chicago	2:00	17.25
100Y4hr_Chicago	2:15	11.53
100Y4hr_Chicago	2:30	8.62
100Y4hr_Chicago	2:45	6.87
100Y4hr_Chicago	3:00	5.71
100Y4hr_Chicago	3:15	4.89
100Y4hr_Chicago	3:30	4.28
100Y4hr_Chicago	3:45	3.81
100Y4hr_Chicago	4:00	0
100YrSCS	0:00	0
100YrSCS	2:00	1.08
100YrSCS	4:00	1.62
100YrSCS	6:00	1.62
100YrSCS	8:00	2.16
100YrSCS	10:00	3.24
100YrSCS	12:00	25.92
100YrSCS	14:00	8.64
100YrSCS	16:00	3.24
100YrSCS	18:00	2.16
100YrSCS	20:00	1.62
100YrSCS	22:00	1.62
100YrSCS	24:00	1.08
5Y4hr_Chicago	0:00	2.58
5Y4hr_Chicago	0:15	3.13
5Y4hr_Chicago	0:30	4.02
5Y4hr_Chicago	0:45	5.66
5Y4hr_Chicago	1:00	9.76
5Y4hr_Chicago	1:15	26.72
5Y4hr_Chicago	1:30	88.4
5Y4hr_Chicago	1:45	18.73
5Y4hr_Chicago	2:00	10.21
5Y4hr_Chicago	2:15	6.99
5Y4hr_Chicago	2:30	5.33
5Y4hr_Chicago	2:45	4.31
5Y4hr_Chicago	3:00	3.64

5Y4hr_Chicago	3:15	3.15
5Y4hr_Chicago	3:30	2.78
5Y4hr_Chicago	3:45	2.49
5Y4hr_Chicago	4:00	0

TW_100YR_24Hr_NorthNeighbourhood	7/7/2017	0:01	172.199936
TW_100YR_24Hr_NorthNeighbourhood	7/7/2017	0:02	172.197479
TW_100YR_24Hr_NorthNeighbourhood	7/7/2017	0:03	172.188278
TW_100YR_24Hr_NorthNeighbourhood	7/7/2017	0:04	172.178711
TW_100YR_24Hr_NorthNeighbourhood	7/7/2017	0:05	172.181015
TW_100YR_24Hr_NorthNeighbourhood	7/7/2017	0:06	172.194061
TW_100YR_24Hr_NorthNeighbourhood	7/7/2017	0:07	172.204269
TW_100YR_24Hr_NorthNeighbourhood	7/7/2017	0:08	172.207779
TW_100YR_24Hr_NorthNeighbourhood	7/7/2017	0:09	172.208679
TW_100YR_24Hr_NorthNeighbourhood	7/7/2017	0:10	172.210159
TW_100YR_24Hr_NorthNeighbourhood	7/7/2017	0:11	172.212555

.....

Too many data points (2160 in total).

TW_100YR_4Hr_NorthNeighbourhood	7/7/2017	0:01	172.199936
TW_100YR_4Hr_NorthNeighbourhood	7/7/2017	0:02	172.197479
TW_100YR_4Hr_NorthNeighbourhood	7/7/2017	0:03	172.188278
TW_100YR_4Hr_NorthNeighbourhood	7/7/2017	0:04	172.178711
TW_100YR_4Hr_NorthNeighbourhood	7/7/2017	0:05	172.181015
TW_100YR_4Hr_NorthNeighbourhood	7/7/2017	0:06	172.194061
TW_100YR_4Hr_NorthNeighbourhood	7/7/2017	0:07	172.204269
TW_100YR_4Hr_NorthNeighbourhood	7/7/2017	0:08	172.207779
TW_100YR_4Hr_NorthNeighbourhood	7/7/2017	0:09	172.208664
TW_100YR_4Hr_NorthNeighbourhood	7/7/2017	0:10	172.210159
TW_100YR_4Hr_NorthNeighbourhood	7/7/2017	0:11	172.21254

.....

Too many data points (2160 in total).

TW_5YR_4Hr_NorthNeighbourHood	7/7/2017	0:01	172.199936
TW_5YR_4Hr_NorthNeighbourHood	7/7/2017	0:02	172.197479
TW_5YR_4Hr_NorthNeighbourHood	7/7/2017	0:03	172.188278
TW_5YR_4Hr_NorthNeighbourHood	7/7/2017	0:04	172.178711
TW_5YR_4Hr_NorthNeighbourHood	7/7/2017	0:05	172.181015
TW_5YR_4Hr_NorthNeighbourHood	7/7/2017	0:06	172.194061
TW_5YR_4Hr_NorthNeighbourHood	7/7/2017	0:07	172.204269
TW_5YR_4Hr_NorthNeighbourHood	7/7/2017	0:08	172.207779



TW_5YR_4Hr_NorthNeighbourHood	7/7/2017	0:09	172.208664
TW_5YR_4Hr_NorthNeighbourHood	7/7/2017	0:10	172.210159
TW_5YR_4Hr_NorthNeighbourHood	7/7/2017	0:11	172.21254

.....

Too many data points (2160 in total).

TW_UST_NorthNeighbourhood	7/7/2017	0:01	172.199936
TW_UST_NorthNeighbourhood	7/7/2017	0:02	172.197479
TW_UST_NorthNeighbourhood	7/7/2017	0:03	172.188278
TW_UST_NorthNeighbourhood	7/7/2017	0:04	172.178711
TW_UST_NorthNeighbourhood	7/7/2017	0:05	172.181015
TW_UST_NorthNeighbourhood	7/7/2017	0:06	172.194061
TW_UST_NorthNeighbourhood	7/7/2017	0:07	172.204269
TW_UST_NorthNeighbourhood	7/7/2017	0:08	172.207779
TW_UST_NorthNeighbourhood	7/7/2017	0:09	172.208679
TW_UST_NorthNeighbourhood	7/7/2017	0:10	172.210159
TW_UST_NorthNeighbourhood	7/7/2017	0:11	172.212555

.....

Too many data points (2160 in total).

UST	0:00	2.41
UST	0:15	2.43
UST	0:30	2.45
UST	0:45	2.46
UST	1:00	2.48
UST	1:15	2.51
UST	1:30	2.53
UST	1:45	2.55
UST	2:00	2.58
UST	2:15	2.61
UST	2:30	2.64
UST	2:45	2.67
UST	3:00	2.71
UST	3:15	2.74
UST	3:30	2.79
UST	3:45	2.83
UST	4:00	2.88
UST	4:15	2.94
UST	4:30	3
UST	4:45	3.07
UST	5:00	3.15

UST	5:15	3.23
UST	5:30	3.33
UST	5:45	3.45
UST	6:00	3.59
UST	6:15	3.75
UST	6:30	3.94
UST	6:45	4.18
UST	7:00	4.49
UST	7:15	4.89
UST	7:30	5.43
UST	7:45	6.2
UST	8:00	7.41
UST	8:15	9.56
UST	8:30	14.29
UST	8:45	32.01
UST	9:00	145.13
UST	9:15	48.51
UST	9:30	23.13
UST	9:45	15.08
UST	10:00	11.35
UST	10:15	9.23
UST	10:30	7.88
UST	10:45	6.94
UST	11:00	6.25
UST	11:15	5.73
UST	11:30	5.32
UST	11:45	4.99
UST	12:00	4.72
UST	12:15	4.49
UST	12:30	4.29
UST	12:45	4.12
UST	13:00	3.98
UST	13:15	3.85
UST	13:30	3.74
UST	13:45	3.63
UST	14:00	3.54
UST	14:15	3.46
UST	14:30	3.39
UST	14:45	3.32
UST	15:00	3.26
UST	15:15	3.2

UST	15:30	3.15
UST	15:45	3.1
UST	16:00	3.05
UST	16:15	3.01
UST	16:30	2.97
UST	16:45	2.93
UST	17:00	2.9
UST	17:15	2.87
UST	17:30	2.84
UST	17:45	2.81
UST	18:00	2.78
UST	18:15	2.76
UST	18:30	2.73
UST	18:45	2.71
UST	19:00	2.69
UST	19:15	2.67
UST	19:30	2.65
UST	19:45	2.63
UST	20:00	2.61
UST	20:15	2.59
UST	20:30	2.57
UST	20:45	2.56
UST	21:00	2.54
UST	21:15	2.53
UST	21:30	2.51
UST	21:45	2.5
UST	22:00	2.49
UST	22:15	2.47
UST	22:30	2.46
UST	22:45	2.45
UST	23:00	2.44
UST	23:15	2.43
UST	23:30	2.42
UST	23:45	2.41

[REPORT]

;;Reporting Options

INPUT YES

CONTROLS NO

SUBCATCHMENTS ALL

NODES ALL

LINKS ALL

[TAGS]

[MAP]

DIMENSIONS	342302.36655	4688537.6191	342475.84645	4688730.7109
UNITS	Meters			

[COORDINATES]

;;Node	X-Coord	Y-Coord
;;-----	-----	-----
SMMH1	342456.582	4688564.669
SMOF1	342457.961	4688556.396
SMS1	342448.335	4688573.265

[VERTICES]

;;Link	X-Coord	Y-Coord
;;-----	-----	-----

[POLYGONS]

;;Subcatchment	X-Coord	Y-Coord
;;-----	-----	-----
SM1	342310.252	4688705.953
SM1	342436.212	4688721.934
SM1	342459.906	4688562.512
SM1	342328.134	4688594.746
SM1	342310.252	4688705.953

[SYMBOLS]

;;Gage	X-Coord	Y-Coord
;;-----	-----	-----

# PCSWMM Post-Development Report: 1:5 year 4 hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

\*\*\*\*\*

## Element Count

\*\*\*\*\*

Number of rain gages ..... 4  
 Number of subcatchments ... 1  
 Number of nodes ..... 3  
 Number of links ..... 2  
 Number of pollutants ..... 0  
 Number of land uses ..... 0

\*\*\*\*\*

## Raingage Summary

\*\*\*\*\*

Name	Data Source	Data Type	Recording Interval
100Y4hr_Chicago	100Y4hr_Chicago	INTENSITY	15 min.
100YrSCS	100YrSCS	INTENSITY	120 min.
5Y4hr_Chicago	5Y4hr_Chicago	INTENSITY	15 min.
UST	UST	INTENSITY	15 min.

\*\*\*\*\*

## Subcatchment Summary

\*\*\*\*\*

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
SM1	1.66	107.10	90.00	1.5000	5Y4hr_Chicago	SMS1

\*\*\*\*\*

## Node Summary

\*\*\*\*\*

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
------	------	--------------	------------	-------------	-----------------

SMMH1	JUNCTION	173.52	1.98	0.0
SMOF1	OUTFALL	171.75	2.13	0.0
SMS1	STORAGE	173.52	1.98	0.0

\*\*\*\*\*  
Link Summary  
\*\*\*\*\*

Name	From Node	To Node	Type	Length	%Slope	Roughness
SMC1	SMMH1	SMOF1	CONDUIT	10.0	2.0004	0.0130
SMO1	SMS1	SMMH1	ORIFICE			

\*\*\*\*\*  
Cross Section Summary  
\*\*\*\*\*

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow
SMC1	CIRCULAR	0.56	0.25	0.14	0.56	1	739.87

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
\*\*\*\*\*

\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... LPS  
Process Models:  
  Rainfall/Runoff ..... YES  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... YES

Ponding Allowed ..... NO  
 Water Quality ..... NO  
 Infiltration Method ..... MODIFIED\_GREEN\_AMPT  
 Flow Routing Method ..... DYNWAVE  
 Surcharge Method ..... EXTRAN  
 Starting Date ..... 10/13/2022 00:00:00  
 Ending Date ..... 10/14/2022 00:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:01:00  
 Wet Time Step ..... 00:05:00  
 Dry Time Step ..... 00:05:00  
 Routing Time Step ..... 5.00 sec  
 Variable Time Step ..... YES  
 Maximum Trials ..... 8  
 Number of Threads ..... 1  
 Head Tolerance ..... 0.001500 m

	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Total Precipitation .....	0.082	49.475
Evaporation Loss .....	0.000	0.000
Infiltration Loss .....	0.005	2.863
Surface Runoff .....	0.074	44.643
Final Storage .....	0.004	2.255
Continuity Error (%) .....	-0.577	

	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	0.074	0.741
Groundwater Inflow .....	0.000	0.000
RDII Inflow .....	0.000	0.000
External Inflow .....	0.000	0.000
External Outflow .....	0.074	0.738
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000

```
*****
Time-Step Critical Elements
*****
Link SMC1 (23.69%)
```

```
*****
Routing Time Step Summary
*****
```

\*\*\*\*\*  
Subcatchment Runoff Summary  
\*\*\*\*\*

		Flow (cfs)						
		1990		2000		2010		2020
Peak	Runoff	Total	Imperv	Total	Imperv	Total	Imperv	Total
1.0	1.0	1.0	0.0	1.0	0.0	1.0	0.0	1.0
2.0	2.0	2.0	0.0	2.0	0.0	2.0	0.0	2.0
3.0	3.0	3.0	0.0	3.0	0.0	3.0	0.0	3.0
4.0	4.0	4.0	0.0	4.0	0.0	4.0	0.0	4.0
5.0	5.0	5.0	0.0	5.0	0.0	5.0	0.0	5.0
6.0	6.0	6.0	0.0	6.0	0.0	6.0	0.0	6.0
7.0	7.0	7.0	0.0	7.0	0.0	7.0	0.0	7.0
8.0	8.0	8.0	0.0	8.0	0.0	8.0	0.0	8.0
9.0	9.0	9.0	0.0	9.0	0.0	9.0	0.0	9.0
10.0	10.0	10.0	0.0	10.0	0.0	10.0	0.0	10.0
11.0	11.0	11.0	0.0	11.0	0.0	11.0	0.0	11.0
12.0	12.0	12.0	0.0	12.0	0.0	12.0	0.0	12.0
13.0	13.0	13.0	0.0	13.0	0.0	13.0	0.0	13.0
14.0	14.0	14.0	0.0	14.0	0.0	14.0	0.0	14.0
15.0	15.0	15.0	0.0	15.0	0.0	15.0	0.0	15.0
16.0	16.0	16.0	0.0	16.0	0.0	16.0	0.0	16.0
17.0	17.0	17.0	0.0	17.0	0.0	17.0	0.0	17.0
18.0	18.0	18.0	0.0	18.0	0.0	18.0	0.0	18.0
19.0	19.0	19.0	0.0	19.0	0.0	19.0	0.0	19.0
20.0	20.0	20.0	0.0	20.0	0.0	20.0	0.0	20.0
21.0	21.0	21.0	0.0	21.0	0.0	21.0	0.0	21.0
22.0	22.0	22.0	0.0	22.0	0.0	22.0	0.0	22.0
23.0	23.0	23.0	0.0	23.0	0.0	23.0	0.0	23.0
24.0	24.0	24.0	0.0	24.0	0.0	24.0	0.0	24.0
25.0	25.0	25.0	0.0	25.0	0.0	25.0	0.0	25.0
26.0	26.0	26.0	0.0	26.0	0.0	26.0	0.0	26.0
27.0	27.0	27.0	0.0	27.0	0.0	27.0	0.0	27.0
28.0	28.0	28.0	0.0	28.0	0.0	28.0	0.0	28.0
29.0	29.0	29.0	0.0	29.0	0.0	29.0	0.0	29.0
30.0	30.0	30.0	0.0	30.0	0.0	30.0	0.0	30.0
31.0	31.0	31.0	0.0	31.0	0.0	31.0	0.0	31.0
32.0	32.0	32.0	0.0	32.0	0.0	32.0	0.0	32.0
33.0	33.0	33.0	0.0	33.0	0.0	33.0	0.0	33.0
34.0	34.0	34.0	0.0	34.0	0.0	34.0	0.0	34.0
35.0	35.0	35.0	0.0	35.0	0.0	35.0	0.0	35.0
36.0	36.0	36.0	0.0	36.0	0.0	36.0	0.0	36.0
37.0	37.0	37.0	0.0	37.0	0.0	37.0	0.0	37.0
38.0	38.0	38.0	0.0	38.0	0.0	38.0	0.0	38.0
39.0	39.0	39.0	0.0	39.0	0.0	39.0	0.0	39.0
40.0	40.0	40.0	0.0	40.0	0.0	40.0	0.0	40.0
41.0	41.0	41.0	0.0	41.0	0.0	41.0	0.0	41.0
42.0	42.0	42.0	0.0	42.0	0.0	42.0	0.0	42.0
43.0	43.0							



Runoff	Coeff	Precip	Runon	Evap	Infil	Runoff	Runoff	Runoff	Runoff
Subcatchment		mm	mm	mm	mm	mm	mm	mm	10^6 ltr
LPS									
-----									
SM1		49.48	0.00	0.00	2.86	42.51	2.13	44.64	0.74
389.54	0.902								

\*\*\*\*\*  
Node Depth Summary  
\*\*\*\*\*

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
SMMH1	JUNCTION	0.03	0.16	173.69	0 01:54	0.16
SMOF1	OUTFALL	1.04	1.04	172.80	0 00:00	1.04
SMS1	STORAGE	0.10	1.35	174.87	0 01:54	1.29

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

Node	Type	Maximum Lateral Inflow LPS	Maximum Total Inflow LPS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 ltr	Total Inflow Volume 10^6 ltr	Flow Balance Error Percent
SMMH1	JUNCTION	0.00	130.51	0 01:54	0	0.738	0.000
SMOF1	OUTFALL	0.00	130.80	0 01:54	0	0.738	0.000
SMS1	STORAGE	389.54	389.54	0 01:45	0.741	0.741	0.008

\*\*\*\*\*  
Node Surcharge Summary

\*\*\*\*\*

No nodes were surcharged.

\*\*\*\*\*

Node Flooding Summary

\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*

Storage Volume Summary

\*\*\*\*\*

Storage Unit	Average Volume 1000 m3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m3	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow LPS
SMS1	0.057	5	0	0	0.386	36	0 01:54	130.51

\*\*\*\*\*

Outfall Loading Summary

\*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow LPS	Max Flow LPS	Total Volume 10^6 ltr
SMOF1	96.46	13.88	130.80	0.738
System	96.46	13.88	130.80	0.738

\*\*\*\*\*

Link Flow Summary

\*\*\*\*\*

Link	Type	Maximum  Flow  LPS	Time of Max Occurrence days hr:min	Maximum  Veloc  m/sec	Max/ Full Flow	Max/ Full Depth
SMC1	CONDUIT	130.80	0 01:54	2.23	0.18	0.28
SMO1	ORIFICE	130.51	0 01:54			1.00

\*\*\*\*\*  
Flow Classification Summary  
\*\*\*\*\*

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								
		Up Dry	Down Dry	Sub Dry	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl	
SMC1	1.00	0.03	0.00	0.00	0.00	0.00	0.00	0.97	0.00	0.00

\*\*\*\*\*  
Conduit Surcharge Summary  
\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Fri Nov 18 16:37:14 2022  
Analysis ended on: Fri Nov 18 16:37:14 2022  
Total elapsed time: < 1 sec

# PCSWMM Output Report 1:100 yr 4 hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

\*\*\*\*\*

Element Count

\*\*\*\*\*

Number of rain gages ..... 4

Number of subcatchments ... 1

Number of nodes ..... 3

Number of links ..... 2

Number of pollutants ..... 0

Number of land uses ..... 0

\*\*\*\*\*

Raingage Summary

\*\*\*\*\*

Name	Data Source	Data Type	Recording Interval
100Y4hr_Chicago	100Y4hr_Chicago	INTENSITY	15 min.
100YrSCS	100YrSCS	INTENSITY	120 min.
5Y4hr_Chicago	5Y4hr_Chicago	INTENSITY	15 min.
UST	UST	INTENSITY	15 min.

\*\*\*\*\*

Subcatchment Summary

\*\*\*\*\*

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
S1	1.66	107.10	90.00	1.5000	100Y4hr_Chicago	1

\*\*\*\*\*

Node Summary

\*\*\*\*\*

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
------	------	--------------	------------	-------------	-----------------

2	JUNCTION	173.52	1.98	0.0
3	OUTFALL	171.75	2.13	0.0
1	STORAGE	173.52	1.98	0.0

\*\*\*\*\*  
Link Summary  
\*\*\*\*\*

Name	From Node	To Node	Type	Length	%Slope	Roughness
2	2	3	CONDUIT	10.0	2.0004	0.0130
1	1	2	ORIFICE			

\*\*\*\*\*  
Cross Section Summary  
\*\*\*\*\*

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow
2	CIRCULAR	0.56	0.25	0.14	0.56	1	739.87

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
\*\*\*\*\*

\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... LPS  
Process Models:  
  Rainfall/Runoff ..... YES  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... YES

Ponding Allowed ..... NO  
 Water Quality ..... NO  
 Infiltration Method ..... MODIFIED\_GREEN\_AMPT  
 Flow Routing Method ..... DYNWAVE  
 Surcharge Method ..... EXTRAN  
 Starting Date ..... 10/13/2022 00:00:00  
 Ending Date ..... 10/14/2022 00:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:01:00  
 Wet Time Step ..... 00:05:00  
 Dry Time Step ..... 00:05:00  
 Routing Time Step ..... 5.00 sec  
 Variable Time Step ..... YES  
 Maximum Trials ..... 8  
 Number of Threads ..... 1  
 Head Tolerance ..... 0.001500 m

*****	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Total Precipitation .....	0.135	81.588
Evaporation Loss .....	0.000	0.000
Infiltration Loss .....	0.005	3.079
Surface Runoff .....	0.127	76.709
Final Storage .....	0.004	2.255
Continuity Error (%) .....	-0.558	

*****	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	0.127	1.272
Groundwater Inflow .....	0.000	0.000
RDII Inflow .....	0.000	0.000
External Inflow .....	0.000	0.000
External Outflow .....	0.125	1.248
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000



Runoff	Coeff	Precip	Runon	Evap	Infil	Runoff	Runoff	Runoff	Runoff
Subcatchment		mm	mm	mm	mm	mm	mm	mm	10^6 ltr
LPS									
-----									
S1		81.59	0.00	0.00	3.08	71.57	5.14	76.71	1.27
651.88	0.940								

\*\*\*\*\*  
Node Depth Summary  
\*\*\*\*\*

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
-----						
2	JUNCTION	0.04	0.21	173.73	0 01:39	0.18
3	OUTFALL	1.78	1.78	173.53	0 00:00	1.78
1	STORAGE	0.25	1.87	175.40	0 02:00	1.87

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

Node	Type	Maximum Lateral Inflow LPS	Maximum Total Inflow LPS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 ltr	Total Inflow Volume 10^6 ltr	Flow Balance Error Percent
-----							
2	JUNCTION	0.00	155.68	0 02:00	0	1.25	-0.002
3	OUTFALL	0.00	166.39	0 01:39	0	1.25	0.000
1	STORAGE	651.88	651.88	0 01:45	1.27	1.27	1.462

\*\*\*\*\*  
Node Surcharge Summary



\*\*\*\*\*

No nodes were surcharged.

\*\*\*\*\*

Node Flooding Summary

\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*

Storage Volume Summary

\*\*\*\*\*

Storage Unit	Average Volume 1000 m3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m3	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow LPS
1	0.094	9	0	0	0.672	63	0 02:00	155.68

\*\*\*\*\*

Outfall Loading Summary

\*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow LPS	Max Flow LPS	Total Volume 10^6 ltr
3	60.09	39.09	166.39	1.248
System	60.09	39.09	166.39	1.248

\*\*\*\*\*

Link Flow Summary

\*\*\*\*\*

Link	Type	Maximum  Flow  LPS	Time of Max Occurrence days hr:min	Maximum  Veloc  m/sec	Max/ Full Flow	Max/ Full Depth
2	CONDUIT	166.39	0 01:39	2.14	0.22	0.37
1	ORIFICE	155.68	0 02:00			1.00

\*\*\*\*\*  
Flow Classification Summary  
\*\*\*\*\*

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								
		Dry	Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl
2	1.00	0.00	0.00	0.00	0.85	0.15	0.00	0.00	0.35	0.00

\*\*\*\*\*  
Conduit Surcharge Summary  
\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Fri Nov 18 16:37:36 2022  
Analysis ended on: Fri Nov 18 16:37:37 2022  
Total elapsed time: 00:00:01

# PCSWMM Output Report: 1:100 yr 24 hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

\*\*\*\*\*

## Element Count

\*\*\*\*\*

Number of rain gages ..... 4  
Number of subcatchments ... 1  
Number of nodes ..... 3  
Number of links ..... 2  
Number of pollutants ..... 0  
Number of land uses ..... 0

\*\*\*\*\*

## Raingage Summary

\*\*\*\*\*

Name	Data Source	Data Type	Recording Interval
100Y4hr_Chicago	100Y4hr_Chicago	INTENSITY	15 min.
100YrSCS	100YrSCS	INTENSITY	120 min.
5Y4hr_Chicago	5Y4hr_Chicago	INTENSITY	15 min.
UST	UST	INTENSITY	15 min.

\*\*\*\*\*

## Subcatchment Summary

\*\*\*\*\*

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
S1	1.66	107.10	90.00	1.5000	100YrSCS	1

\*\*\*\*\*

## Node Summary

\*\*\*\*\*

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
------	------	--------------	------------	-------------	-----------------

2	JUNCTION	173.52	1.98	0.0
3	OUTFALL	171.75	2.13	0.0
1	STORAGE	173.52	1.98	0.0

\*\*\*\*\*

#### Link Summary

\*\*\*\*\*

Name	From Node	To Node	Type	Length	%Slope	Roughness
2	2	3	CONDUIT	10.0	2.0004	0.0130
1	1	2	ORIFICE			

\*\*\*\*\*

#### Cross Section Summary

\*\*\*\*\*

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow
2	CIRCULAR	0.56	0.25	0.14	0.56	1	739.87

\*\*\*\*\*

NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.

\*\*\*\*\*

\*\*\*\*\*

#### Analysis Options

\*\*\*\*\*

Flow Units ..... LPS

#### Process Models:

Rainfall/Runoff ..... YES  
RDII ..... NO  
Snowmelt ..... NO  
Groundwater ..... NO  
Flow Routing ..... YES

Ponding Allowed ..... NO  
 Water Quality ..... NO  
 Infiltration Method ..... MODIFIED\_GREEN\_AMPT  
 Flow Routing Method ..... DYNWAVE  
 Surcharge Method ..... EXTRAN  
 Starting Date ..... 10/13/2022 00:00:00  
 Ending Date ..... 10/14/2022 00:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:01:00  
 Wet Time Step ..... 00:05:00  
 Dry Time Step ..... 00:05:00  
 Routing Time Step ..... 5.00 sec  
 Variable Time Step ..... YES  
 Maximum Trials ..... 8  
 Number of Threads ..... 1  
 Head Tolerance ..... 0.001500 m

	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Total Precipitation .....	0.176	105.840
Evaporation Loss .....	0.000	0.000
Infiltration Loss .....	0.009	5.373
Surface Runoff .....	0.161	97.227
Final Storage .....	0.006	3.364
Continuity Error (%) .....	-0.117	

	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	0.161	1.613
Groundwater Inflow .....	0.000	0.000
RDII Inflow .....	0.000	0.000
External Inflow .....	0.000	0.000
External Outflow .....	0.137	1.367
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000

```
*****
Time-Step Critical Elements
*****
Link 2 (63.81%)
```

```
*****
Routing Time Step Summary
*****
```

\*\*\*\*\*  
Subcatchment Runoff Summary  
\*\*\*\*\*

		Total	Total	Total	Total	Imperv	Perv	Total
Peak	Runoff							Total

Runoff	Coeff	Precip	Runon	Evap	Infil	Runoff	Runoff	Runoff	Runoff
Subcatchment		mm	mm	mm	mm	mm	mm	mm	10^6 ltr
LPS									
-----									
S1		105.84	0.00	0.00	5.37	92.42	4.81	97.23	1.61
117.91	0.919								

\*\*\*\*\*  
Node Depth Summary  
\*\*\*\*\*

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
-----						
2	JUNCTION	0.31	0.44	173.97	0 12:44	0.43
3	OUTFALL	2.19	2.19	173.95	0 00:00	2.19
1	STORAGE	0.42	1.39	174.92	0 14:00	1.39

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

Node	Type	Maximum Lateral Inflow LPS	Maximum Total Inflow LPS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 ltr	Total Inflow Volume 10^6 ltr	Flow Balance Error Percent
-----							
2	JUNCTION	0.00	117.91	0 14:00	0	1.37	0.038
3	OUTFALL	0.00	117.91	0 14:00	0	1.37	0.000
1	STORAGE	117.91	117.91	0 14:00	1.61	1.61	0.117

\*\*\*\*\*  
Node Surcharge Summary

\*\*\*\*\*

No nodes were surcharged.

\*\*\*\*\*

Node Flooding Summary

\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*

Storage Volume Summary

\*\*\*\*\*

Storage Unit	Average Volume 1000 m3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m3	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow LPS
1	0.206	19	0	0	0.386	36	0 14:00	117.91

\*\*\*\*\*

Outfall Loading Summary

\*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow LPS	Max Flow LPS	Total Volume 10^6 ltr
3	63.86	33.82	117.91	1.367
System	63.86	33.82	117.91	1.367

\*\*\*\*\*

Link Flow Summary

\*\*\*\*\*



Link	Type	Maximum  Flow  LPS	Time of Max Occurrence days hr:min	Maximum  Veloc  m/sec	Max/ Full Flow	Max/ Full Depth
2	CONDUIT	117.91	0 14:00	0.51	0.16	0.89
1	ORIFICE	117.91	0 14:00			1.00

\*\*\*\*\*  
Flow Classification Summary  
\*\*\*\*\*

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								
		Up		Down	Sub	Sup	Up	Down	Norm	Inlet
		Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd	Ctrl
2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00

\*\*\*\*\*  
Conduit Surcharge Summary  
\*\*\*\*\*

Conduit	Both Ends	Hours Full		Hours	Hours
		Upstream	Dnstream	Above Full Normal Flow	Capacity Limited
2	0.01	0.01	24.00	0.01	0.01

Analysis begun on: Fri Nov 18 16:38:06 2022  
Analysis ended on: Fri Nov 18 16:38:06 2022  
Total elapsed time: < 1 sec

# PCSWMM Output Report: Urban Stress Test (UST)

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

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\*\*\*\*\*

## Element Count

\*\*\*\*\*

Number of rain gages ..... 4  
Number of subcatchments ... 1  
Number of nodes ..... 3  
Number of links ..... 2  
Number of pollutants ..... 0  
Number of land uses ..... 0

\*\*\*\*\*

## Raingage Summary

\*\*\*\*\*

Name	Data Source	Data Type	Recording Interval
100Y4hr_Chicago	100Y4hr_Chicago	INTENSITY	15 min.
100YrSCS	100YrSCS	INTENSITY	120 min.
5Y4hr_Chicago	5Y4hr_Chicago	INTENSITY	15 min.
UST	UST	INTENSITY	15 min.

\*\*\*\*\*

## Subcatchment Summary

\*\*\*\*\*

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
S1	1.66	107.10	90.00	1.5000	UST	1

\*\*\*\*\*

## Node Summary

\*\*\*\*\*

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
------	------	--------------	------------	-------------	-----------------

2	JUNCTION	173.52	1.98	0.0
3	OUTFALL	171.75	2.13	0.0
1	STORAGE	173.52	1.98	0.0

\*\*\*\*\*

#### Link Summary

\*\*\*\*\*

Name	From Node	To Node	Type	Length	%Slope	Roughness
2	2	3	CONDUIT	10.0	2.0004	0.0130
1	1	2	ORIFICE			

\*\*\*\*\*

#### Cross Section Summary

\*\*\*\*\*

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow
2	CIRCULAR	0.56	0.25	0.14	0.56	1	739.87

\*\*\*\*\*

NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.

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\*\*\*\*\*

#### Analysis Options

\*\*\*\*\*

Flow Units ..... LPS

#### Process Models:

Rainfall/Runoff ..... YES

RDII ..... NO

Snowmelt ..... NO

Groundwater ..... NO

Flow Routing ..... YES

Ponding Allowed ..... NO  
 Water Quality ..... NO  
 Infiltration Method ..... MODIFIED\_GREEN\_AMPT  
 Flow Routing Method ..... DYNWAVE  
 Surcharge Method ..... EXTRAN  
 Starting Date ..... 10/13/2022 00:00:00  
 Ending Date ..... 10/14/2022 00:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:01:00  
 Wet Time Step ..... 00:05:00  
 Dry Time Step ..... 00:05:00  
 Routing Time Step ..... 5.00 sec  
 Variable Time Step ..... YES  
 Maximum Trials ..... 8  
 Number of Threads ..... 1  
 Head Tolerance ..... 0.001500 m

	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Total Precipitation .....	0.249	149.985
Evaporation Loss .....	0.000	0.000
Infiltration Loss .....	0.011	6.509
Surface Runoff .....	0.233	140.077
Final Storage .....	0.007	3.942
Continuity Error (%) .....	-0.362	

	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	0.232	2.324
Groundwater Inflow .....	0.000	0.000
RDII Inflow .....	0.000	0.000
External Inflow .....	0.000	0.000
External Outflow .....	0.193	1.935
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000

Initial Stored Volume ....	0.000	0.001
Final Stored Volume .....	0.039	0.388
Continuity Error (%) .....	0.110	

\*\*\*\*\*  
Time-Step Critical Elements  
\*\*\*\*\*  
None

\*\*\*\*\*  
Highest Flow Instability Indexes  
\*\*\*\*\*  
Link 1 (14)

\*\*\*\*\*  
Routing Time Step Summary  
\*\*\*\*\*

Minimum Time Step	:	4.50 sec
Average Time Step	:	5.00 sec
Maximum Time Step	:	5.00 sec
Percent in Steady State	:	0.00
Average Iterations per Step	:	2.29
Percent Not Converging	:	0.03
Time Step Frequencies	:	
5.000 - 3.155 sec	:	100.00 %
3.155 - 1.991 sec	:	0.00 %
1.991 - 1.256 sec	:	0.00 %
1.256 - 0.792 sec	:	0.00 %
0.792 - 0.500 sec	:	0.00 %

\*\*\*\*\*  
Subcatchment Runoff Summary  
\*\*\*\*\*

-----								
-----								
Peak Runoff	Total	Total	Total	Total	Imperv	Perv	Total	Total

Runoff	Coeff	Precip	Runon	Evap	Infil	Runoff	Runoff	Runoff	Runoff
Subcatchment		mm	mm	mm	mm	mm	mm	mm	10^6 ltr
LPS									
-----									
S1		149.98	0.00	0.00	6.51	132.33	7.74	140.08	2.33
659.75	0.934								

\*\*\*\*\*  
Node Depth Summary  
\*\*\*\*\*

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
2	JUNCTION	0.68	0.95	174.47	0 08:34	0.93
3	OUTFALL	2.69	2.69	174.45	0 00:00	2.69
1	STORAGE	0.81	1.96	175.48	0 09:41	1.96

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

Node	Type	Maximum Lateral Inflow LPS	Maximum Total Inflow LPS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 ltr	Total Inflow Volume 10^6 ltr	Flow Balance Error Percent
2	JUNCTION	0.00	121.44	0 09:41	0	1.94	0.085
3	OUTFALL	0.00	121.44	0 09:41	0	1.93	0.000
1	STORAGE	659.75	659.75	0 09:15	2.32	2.32	0.094

\*\*\*\*\*  
Node Surcharge Summary

\*\*\*\*\*

Surcharging occurs when water rises above the top of the highest conduit.

-----				
Node	Type	Hours Surcharged	Max. Height Above Crown Meters	Min. Depth Below Rim Meters
-----				
2	JUNCTION	15.99	0.383	1.028

\*\*\*\*\*

#### Node Flooding Summary

\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*

#### Storage Volume Summary

\*\*\*\*\*

-----								
Storage Unit	Average Volume 1000 m3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m3	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow LPS
-----								
1	0.338	32	0	0	0.986	93	0 09:41	121.44

\*\*\*\*\*

#### Outfall Loading Summary

\*\*\*\*\*

-----				
Outfall Node	Flow Freq Pcnt	Avg Flow LPS	Max Flow LPS	Total Volume 10^6 ltr
-----				
3	64.27	34.84	121.44	1.935
-----				

System                      64.27        34.84        121.44        1.935

\*\*\*\*\*  
Link Flow Summary  
\*\*\*\*\*

Link	Type	Maximum  Flow  LPS	Time of Max Occurrence days hr:min	Maximum  Veloc  m/sec	Max/ Full Flow	Max/ Full Depth
2	CONDUIT	121.44	0 09:41	0.48	0.16	1.00
1	ORIFICE	121.44	0 09:41			1.00

\*\*\*\*\*  
Flow Classification Summary  
\*\*\*\*\*

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								
		Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl	
2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00

\*\*\*\*\*  
Conduit Surcharge Summary  
\*\*\*\*\*

Conduit	Hours Full			Hours Above Full Normal Flow	Hours Capacity Limited
	Both Ends	Upstream	Dnstream		
2	15.99	15.99	24.00	0.01	0.01

Analysis begun on: Fri Nov 18 16:37:55 2022



Analysis ended on: Fri Nov 18 16:37:55 2022  
Total elapsed time: < 1 sec

## Appendix C

### *Details of OGS Unit*

# ADS OGS Sizing Summary

<b>Project Name:</b>	Riverside Sportsman Club Development	
<b>Consulting Engineer:</b>	Dillon Consulting	
<b>Location:</b>	Windsor, ON	
<b>Sizing Completed By:</b>	C. Neath	<b>Email:</b> <a href="mailto:cody.neath@ads-pipe.com">cody.neath@ads-pipe.com</a>

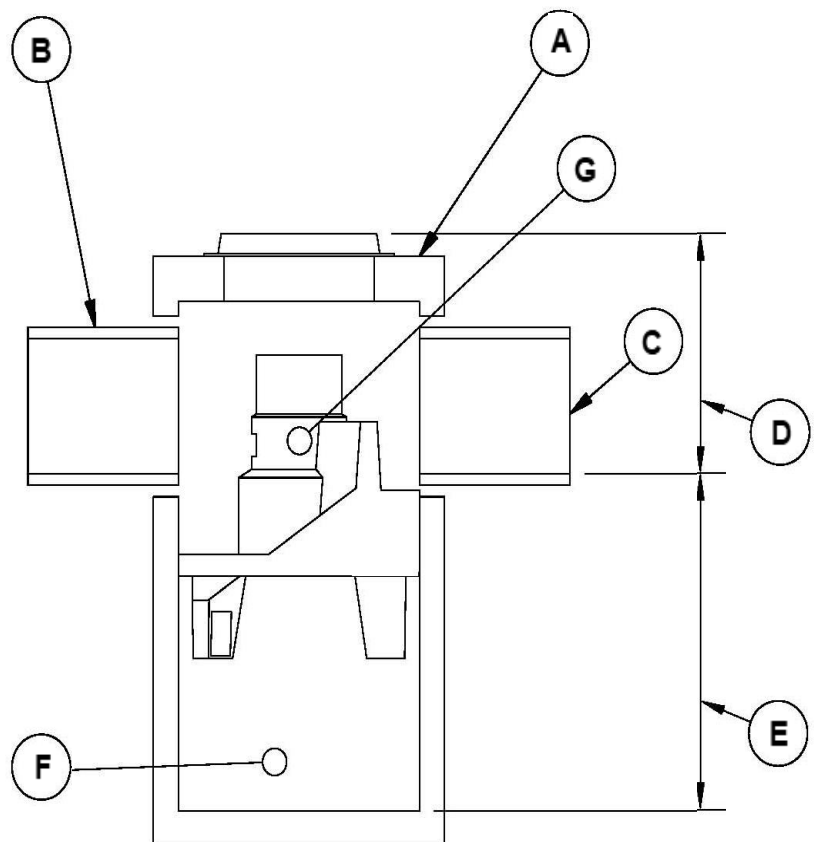
Treatment Requirements		
Treatment Goal:	Normal (MOE)	
Selected Parameters:	70% TSS	90% Volume
Selected Unit:	FD-5HC	

Summary of Results		
Model	TSS Removal	Volume Treated
FD-4HC	59.0%	>90%
FD-5HC	72.0%	>90%
FD-6HC	79.0%	>90%
FD-8HC	84.0%	>90%
FD-10HC	87.0%	>90%

FD-5HC Specification	
Unit Diameter (A):	1,500 mm
Inlet Pipe Diameter (B):	300 mm
Outlet Pipe Diameter (C):	300 mm
Height, T/G to Outlet Invert (D):	2000 mm
Height, Outlet Invert to Sump (E):	1780 mm
Sediment Storage Capacity (F):	1.29 m <sup>3</sup>
Oil Storage Capacity (G):	1,135 L
Recommended Sediment Depth for Maintenance:	475 mm
Max. Pipe Diameter:	600 mm
Peak Flow Capacity:	566 L/s

Site Elevations:	
Rim Elevation:	100.00
Inlet Pipe Elevation:	98.00
Outlet Pipe Elevation:	98.00

Site Details	
Site Area:	1.66 ha
% Impervious:	90%
Rational C:	0.84
Rainfall Station:	Windsor, ONT
Particle Size Distribution:	Fine
Peak Flowrate:	160 L/s



## Notes:

Removal efficiencies are based on NJDEP Test Protocols and independently verified.

All units supplied by ADS have numerous local, provincial, and international certifications (copies of which can be provided upon request). The design engineer is responsible for ensuring compliance with applicable regulations.



Project Name: Riverside Sportsman Club Development  
 Consulting Engineer: Dillon Consulting  
 Location: Windsor, ON

### **Net Annual Removal Efficiency Summary: FD-5HC**

Rainfall Intensity <sup>(1)</sup>	Rational Equation Flowrate	Surface Loading Rate	Fraction of Rainfall <sup>(1)</sup>	FD-5HC Removal Efficiency	Weighted Net-Annual Removal Efficiency
mm/hr	L/s	L/min/m <sup>2</sup>	%	%	%
3.00	11.6	395	13.2%	87%	11.4%
4.00	15.5	526	9.6%	84%	8.1%
5.00	19.4	658	7.5%	83%	6.2%
6.00	23.2	789	6.0%	81%	4.9%
7.00	27.1	921	4.8%	80%	3.8%
8.00	31.0	1052	4.1%	79%	3.2%
9.00	34.9	1184	3.6%	78%	2.8%
10.00	38.7	1315	3.2%	78%	2.5%
11.00	42.6	1447	2.8%	77%	2.2%
12.00	46.5	1578	2.5%	76%	1.9%
15.00	58.1	1973	6.6%	75%	4.9%
20.00	77.5	2630	8.3%	73%	6.0%
25.00	96.8	3288	5.8%	71%	4.1%
30.00	116.2	3945	4.6%	70%	3.2%
35.00	135.6	4603	3.8%	69%	2.6%
40.00	154.9	5260	2.9%	68%	2.0%
45.00	174.3	5918	2.4%	67%	1.6%
50.00	193.7	6576	1.8%	0%	0.0%
65.00	251.8	8548	6.6%	0%	0.0%
<b>Total Net Annual Removal Efficiency:</b>					71.6%
<b>Total Runoff Volume Treated:</b>					99.9%

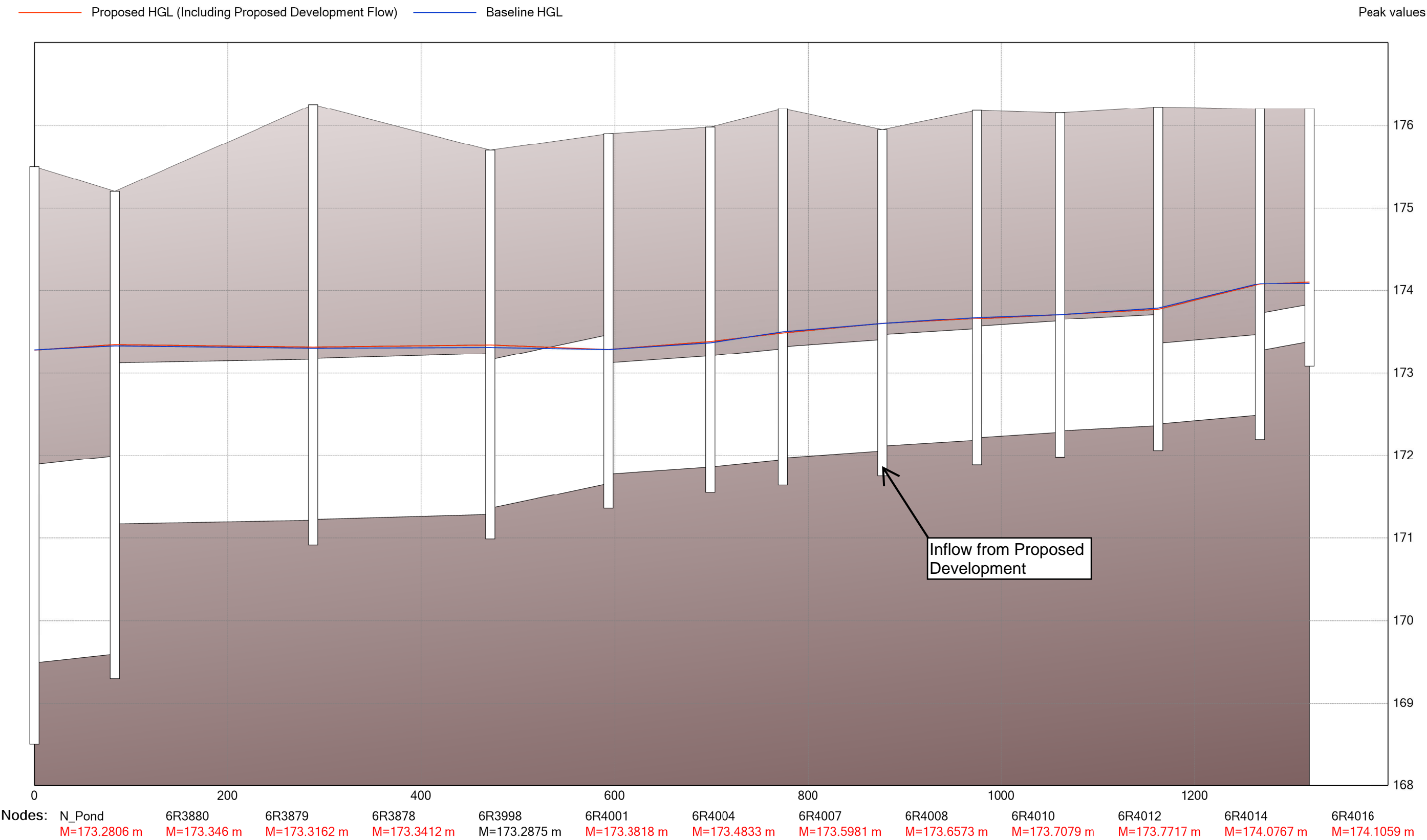
#### **Notes:**

- (1) Based on Windsor/Essex Region Stormwater Manual 2018, Table 3.4.1.5
- (2) Based on third party verified data and approximating the removal of a PSD similar to the STC Fine distribution

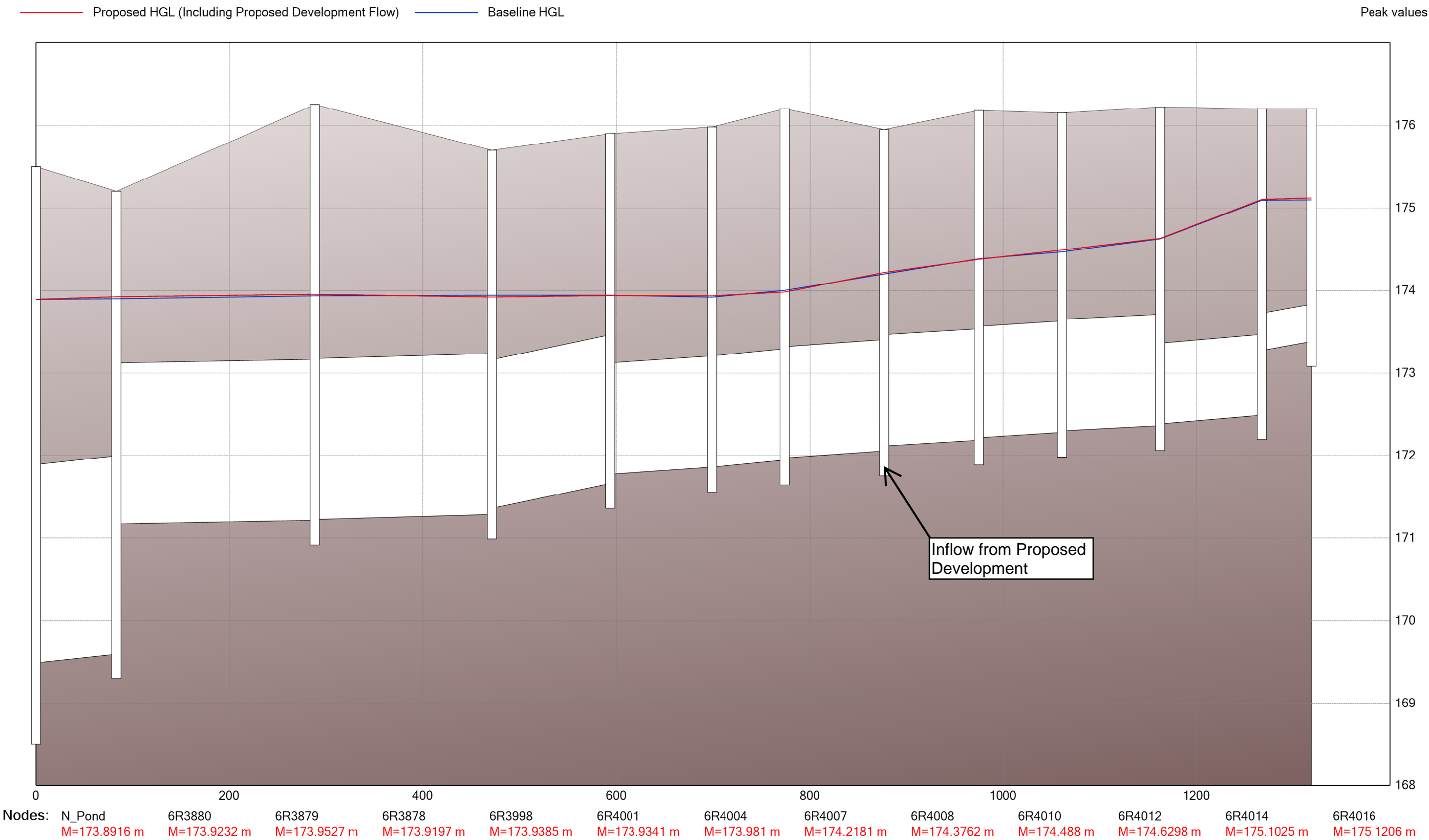
## Appendix D

### *Wyandotte Street East Trunk Sewer Profile Comparison*

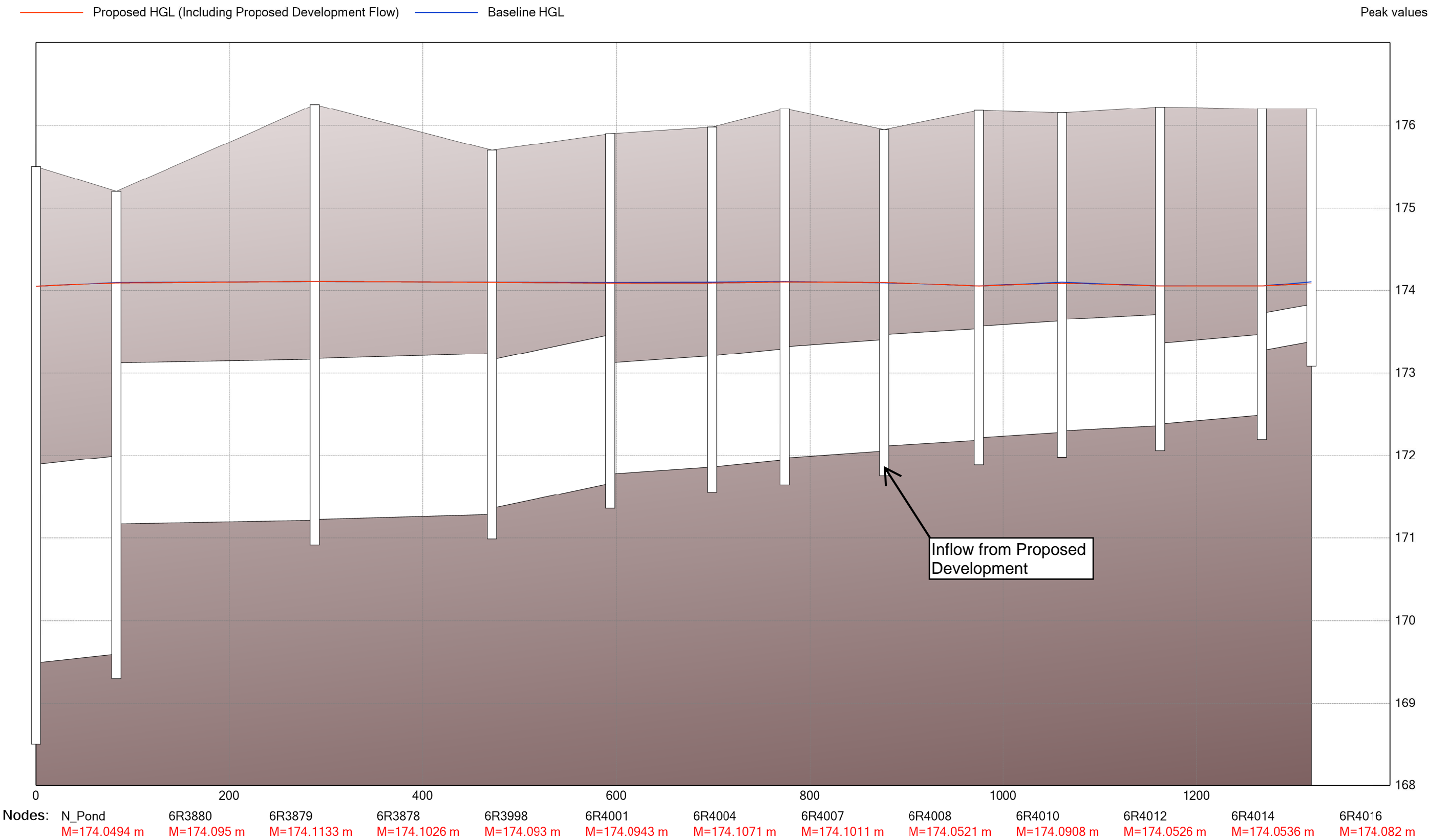
Wyandotte Street East Trunk Sewer HGL Profile Comparison (1:5 year 4 hour)



Wyandotte Street East Trunk Sewer HGL Profile Comparison (1:100 year 4 hour)



Wyandotte Street East Trunk Sewer HGL Profile Comparison (1:100 year 24 hour)





Wyandotte Street East Trunk Sewer HGL Profile Comparison (UST)

